

Evaluation of pump energy consumption for two principles for hydraulic balancing and control of cooling systems



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Evaluation of pump energy consumption for two principles for hydraulic balancing and control of cooling systems

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2. Introduction

FRESE A/S has asked DTI to evaluate two strategies for larger hydraulic cooling systems – in terms of pump energy consumption.

Two examples have been chosen, both using water as cooling fluid:

1. A server room including battery pack and several cooled racks
2. A comfort cooling system with cooled ceiling panels

The strategies considered are:

- Hydraulic balancing using “static” valves + one differential pressure controller for the network. In order to measure and adjust the flow, some pressure drop is needed in the static valves.
- Hydraulic balancing using “dynamic” valves mounted at each cooling device. The dynamic valve is a combined differential pressure controller and control valve. This system is in a wide range independent of the flow and pressure conditions in the network and further valves in the network are not needed.

To quantify the energy consumption some operation profiles are needed. At part load the water flow rapidly decreases. To take this into account the figure 1 is used. The relation between flow and cooling load is calculated based on traditional heat exchanger theory.

The Grundfos product center dimensioning is used for the calculation of annual savings. The Grundfos system allows for user defined load profiles.

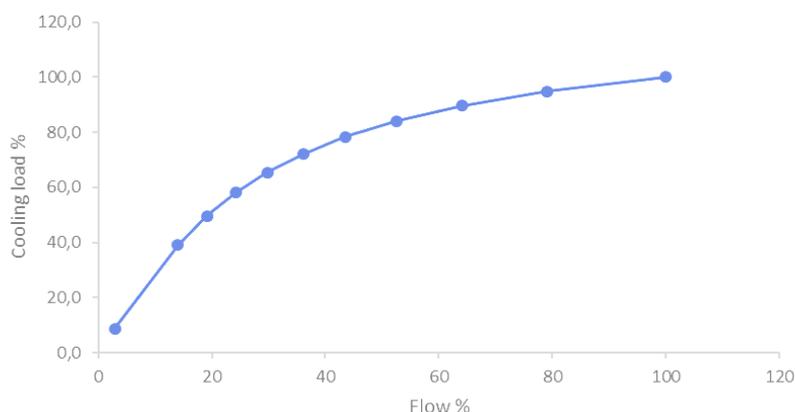


Figure 1 Simplified relation between flow of cooling fluid and cooling load for a server-room-cooler. 50% load needs 20% flow. The calculation of the relation is based on heating up the cooling water by 5 K at max. load and 20 °C in the room. The curve is also assumed to be valid for comfort cooling.

The assumption is that the load differs from day to night, due to the load on server capacity. At 50 % cooling load in the night, the flow is calculated to 20%.



3. Server room

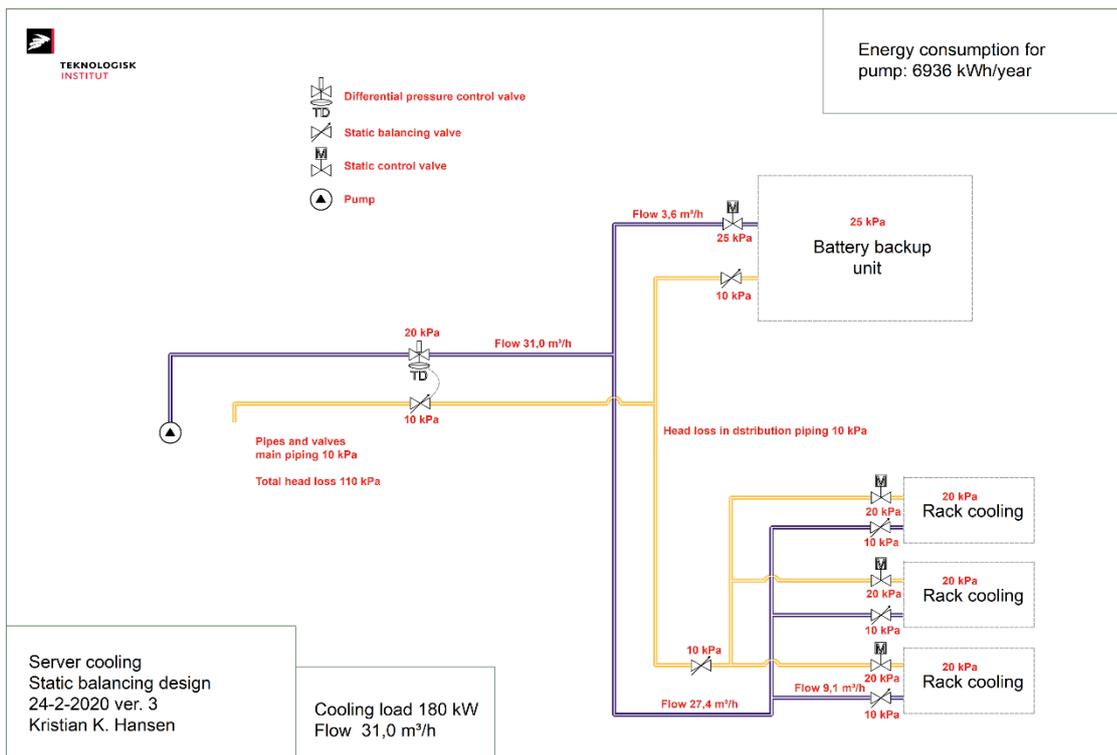


Figure 2 Server room static valves

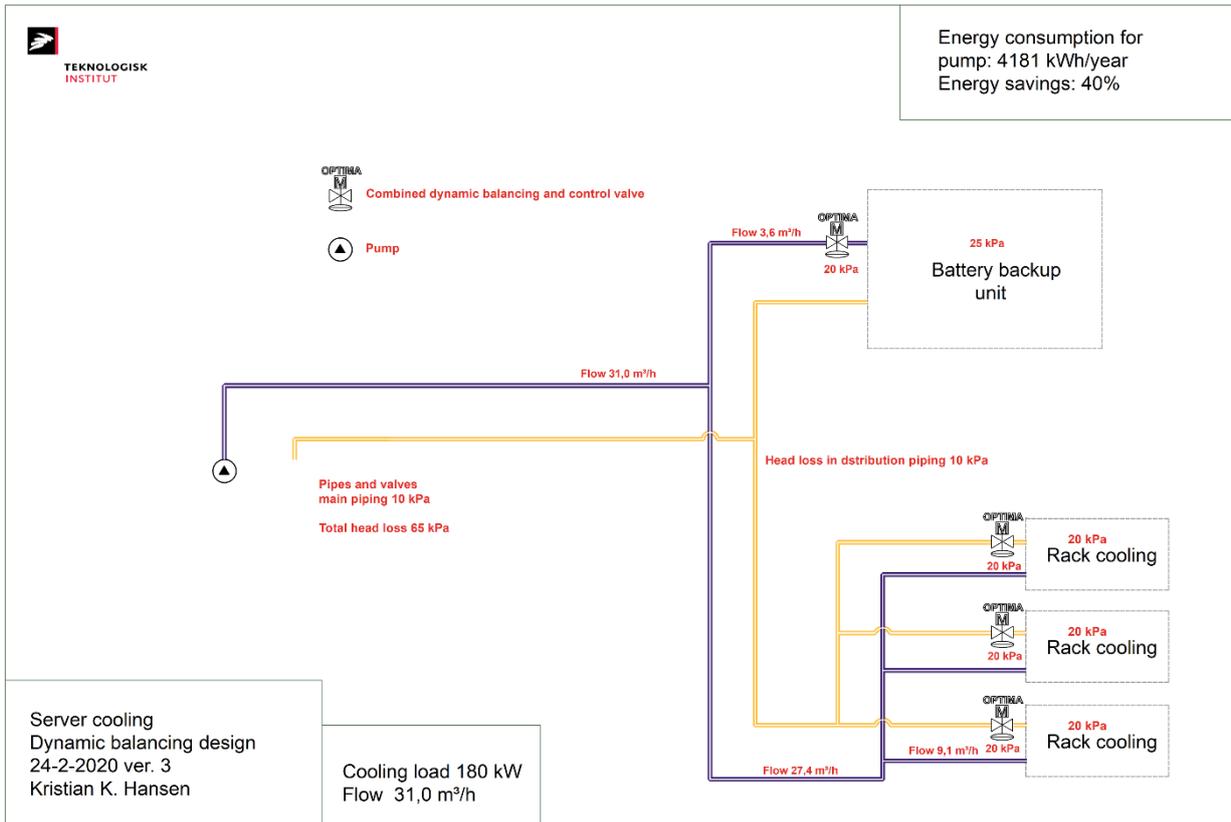


Figure 3 Server room dynamic valves

Sizing result		Load profile		
Type	MAGNA3 65-150F			
Quantity	1		1	2
Motor		Flow	100	20
		Head	100	43
Flow	31 m³/h	P1	1.372	0.211
Head	110 kPa	Eta total	69.0	38.6
Power P1	1.373 kW	Time	4380	4380
Eta pump+motor	69.0 %=Eta pump * Eta motor	Energy consumption	6012	925
Eta total	69.0 %=Eta relative to the duty point	Quantity	1	1
Energy consumption	6936 kWh/Year			
CO2 emission	3950 kg/Year			
Price	28.635,00 DKK			
Life cycle cost	320617 DKK/15Years			

Table 1 Pump selection for the static balanced and controlled system. The part load head is estimated, based on the assumption that the total pressure drop at 20% flow in the pipes and the static valves is negligible, while the pressure drop across the control valve is maintained.



Sizing result		Load profile		
Type	MAGNA3 80-100F			
Quantity	1		1	2
Motor				
Flow	31 m ³ /h	Flow	100	20 %
Head	65 kPa	Head	100	34 %
Power P1	0.859 kW	P1	0.859	0.096 kW
Eta pump+motor	65.2 %=Eta pump * Eta motor	Eta total	65.2	39.5 %
Eta total	65.2 %=Eta relative to the duty point	Time	4380	4380 h/a
Energy consumption	4181 kWh/Year	Energy consumption	3761	420 kWh/Year
CO2 emission	2380 kg/Year	Quantity	1	1
Price	28.810,00 DKK			
Life cycle cost	204826 DKK/15Years			

Table 2 Pump selection for the dynamic balanced and controlled system. The part load head is estimated, based on the assumption that the total pressure drop at 20% flow in the pipes is negligible, while the pressure drop across the control valve is maintained.

Static balanced and controlled	Day	Night	
Load %	100	50	
Flow m ³ /h	31	6,2	
Head kPa	110	47	The calculation shows a pump energy consumption of app. 7000 kWh per year in a static balanced and controlled system for an evenly distributed day and night-time operating cycle.
Operation hours	4380	4380	
kWh/year	6936		

Dynamic balanced and controlled	Day	Night	
Load %	100	50	
Flow m ³ /h	31	6,2	
Head kPa	65	22	The calculation shows a pump energy consumption of app. 4200 kWh per year in a dynamic balanced and controlled system for an evenly distributed day and night-time operating cycle.
Operation hours	4380	4380	
kWh/year	4181		

Table 3 Results for the server room. The pump energy savings are 40 % when changing from static to dynamic balanced and controlled system.



4. Comfort cooling – cooling ceiling

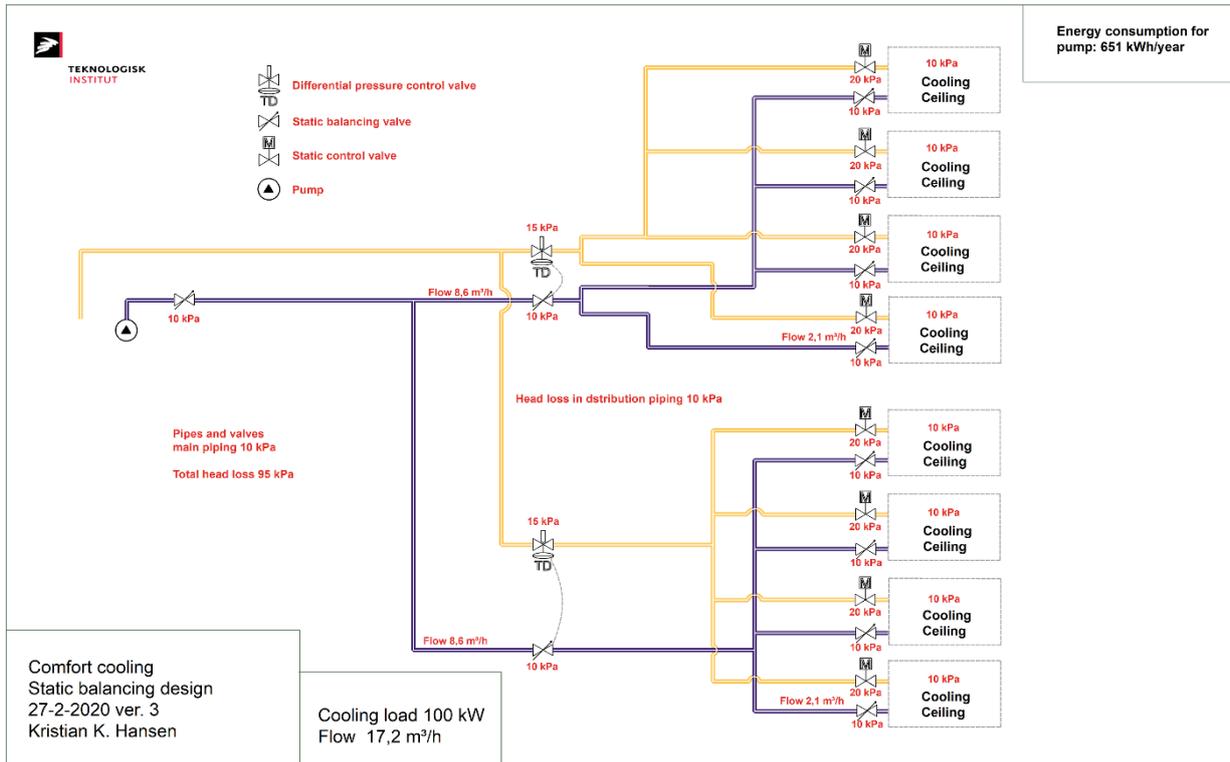


Figure 4 Comfort cooling static valves

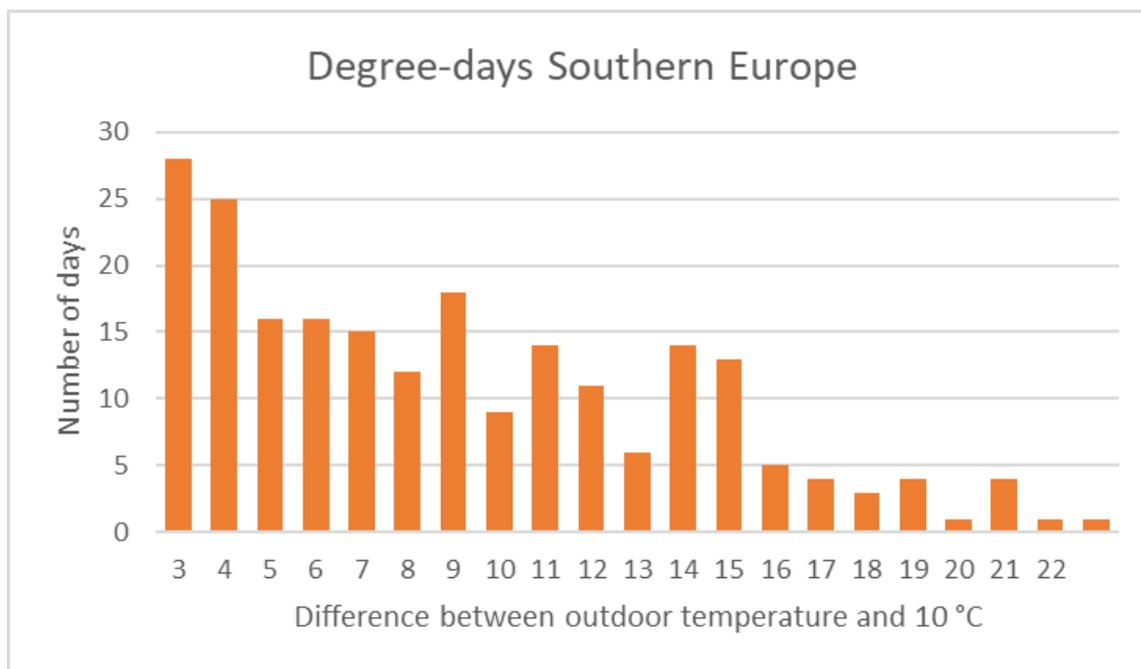


Figure 6 The load distribution is assumed to follow the cooling degree days for Lyon, basis 10 °C, 221 days

	Bin 1					Bin 2							Bin 3						Bin 4		
Degrees	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23
Days	28	25	16	16	15	12	18	9	14	11	6	14	13	5	4	3	4	1	4	2	1

Table 4 Load distribution divided in 4 bins, 5, 11, 19 and max 23 K temperature difference to a chosen basic temperature of 10 °C

Bin	Delta T	Days	Hours	% load	% Flow	Flow m³/h	Static Bal.	Dynamic Bal.
							Delta P kPa	
1	5	100	2400	21,7	9	1,5	35,5	30,2
2	11	84	2016	47,8	20	3,4	37,4	30,8
3	19	36	864	82,6	50	8,6	50,0	35,0
4 (max)	23	1	24	100,0	100	17,2	95,0	50,0
Min = pressure drop control valves							35,0	30,0
Total		221	5304					

Table 5 Load distribution for the pump, static and dynamic balancing. The flow needed is taken from figure 1.



Sizing result		Load profile			
Type	MAGNA3 50-180F				
Quantity	1		1	2	3
Motor			4		
Flow	17.2 m ³ /h	Flow	9	20	50
Head	95 kPa	Head	37	39	53
Power P1	0.712 kW	P1	0.09	0.112	0.223
Eta pump+motor	63.8 %=Eta pump * Eta motor	Eta total	16.4	31.6	53.5
Eta total	63.8 %=Eta relative to the duty point	Time	2400	2016	864
Energy consumption	651 kWh/Year	Energy consumption	216	225	193
CO2 emission	371 kg/Year	Quantity	1	1	1
Price	27.265,00 DKK				
Life cycle cost	54675 DKK/15Years				

Table 6 Sizing. This pump in a static balanced and controlled system has an annual consumption of 651 kWh/year.

Sizing result		Load profile			
Type	MAGNA3 40-120F				
Quantity	1		1	2	3
Motor			4		
Flow	17.2 m ³ /h	Flow	9	20	50
Head	50 kPa	Head	60	62	70
Power P1	0.391 kW	P1	0.054	0.071	0.138
Eta pump+motor	61.1 %=Eta pump * Eta motor	Eta total	23.4	41.2	60.5
Eta total	61.1 %=Eta relative to the duty point	Time	2400	2016	864
Energy consumption	400 kWh/Year	Energy consumption	129	142	119
CO2 emission	228 kg/Year	Quantity	1	1	1
Price	15.935,00 DKK				
Life cycle cost	32765 DKK/15Years				

Table 7 Sizing. This pump in a dynamic balanced and controlled system has an annual consumption of 400 kWh/year

The conclusion for the cooling ceiling is a reduction in annual consumption for the pump from 651 to 400 kWh, or 39% when changing from a static to a dynamic balanced and controlled system. The gross price of the pump is 41% lower in a dynamic system.

Cooling load controlled by cooling water temperature, assuming a constant flow. This is the other extreme, with no individual control of the ceiling panels.

Sizing result		Load profile	
Type	MAGNA3 50-180F		
Quantity	1		1
Motor		Flow	100 %
Flow	17.2 m ³ /h	Head	100 %
Head	95 kPa	P1	0.711 kW
Power P1	0.712 kW	Eta total	63.8 %
Eta pump+motor	63.8 %=Eta pump * Eta motor	Time	5280 h/a
Eta total	63.8 %=Eta relative to the duty point	Energy consumption	3757 kWh/Year
Energy consumption	3757 kWh/Year	Quantity	1
CO2 emission	2140 kg/Year		
Price	27.265,00 DKK		
Life cycle cost	185396 DKK/15Years		

Table 8 Pump sizing using static balancing in a temperature-controlled cooling system



Sizing result			
Type	MAGNA3 40-120F	Load profile	
Quantity	1		1
Motor		Flow	100 %
		Head	100 %
Flow	17.2 m ³ /h	P1	0.391 kW
Head	50 kPa	Eta total	61.1 %
Power P1	0.391 kW	Time	5280 h/a
Eta pump+motor	61.1 %=Eta pump * Eta motor	Energy consumption	2065 kWh/Year
Eta total	61.1 %=Eta relative to the duty point	Quantity	1
Energy consumption	2065 kWh/Year		
CO2 emission	1180 kg/Year		
Price	15.935,00 DKK		
Life cycle cost	102862 DKK/15Years		

Table 9 Pump sizing using dynamic balancing in a temperature-controlled cooling system

In the above example the pump energy saving is 45 % when changing from a static to a dynamic balanced and controlled system. The gross price of the pump is 41 % lower in a dynamic system.

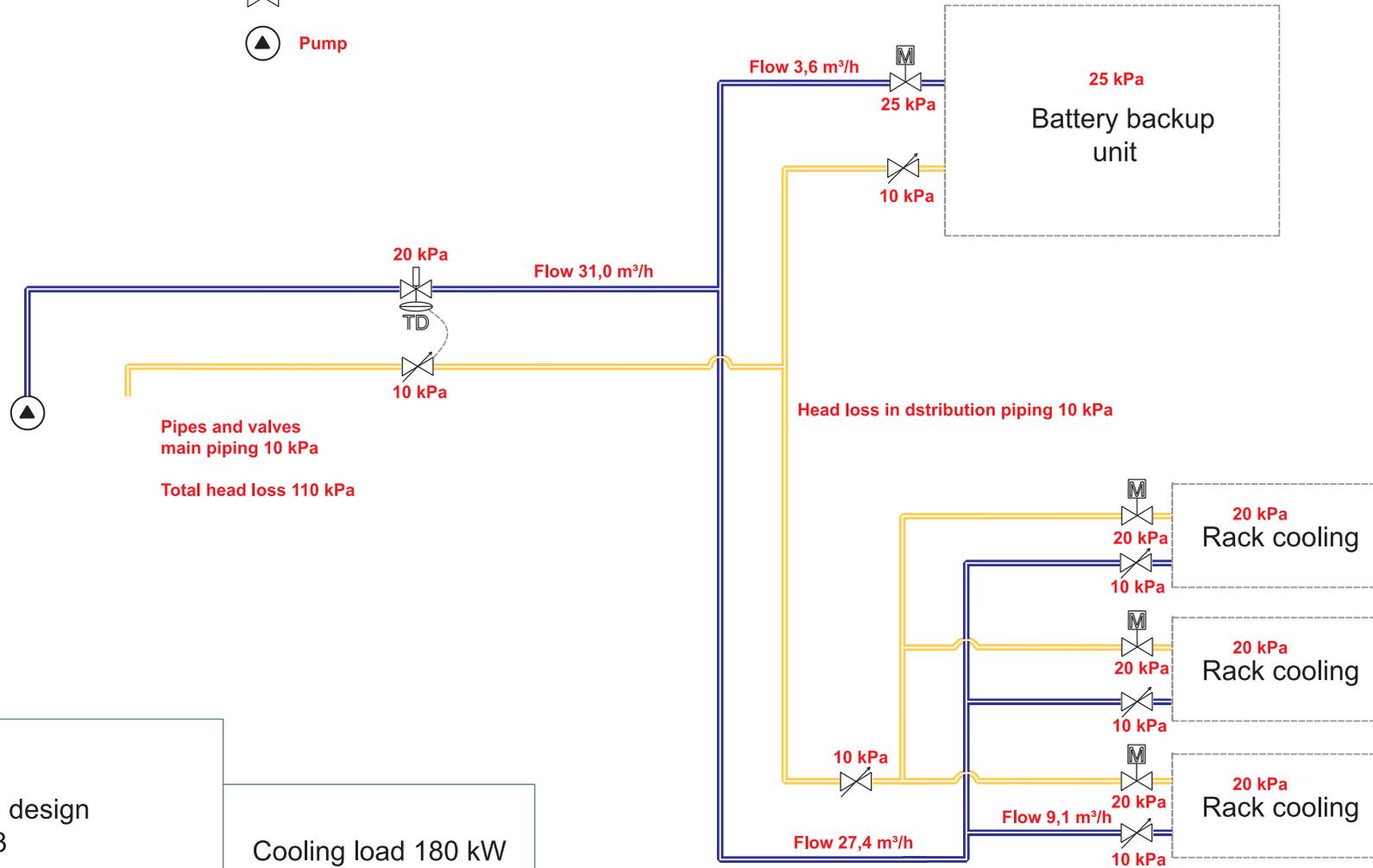
In the practical situation the control of the load will be a combination of flow and temperature control. The pump energy savings will be 40–45%. Flow control of the cooling load reduces the electricity consumption, but for the cooling ceiling there will be considerations concerning minimum flow for some types of panels in order to ensure a correct flow distribution inside the cooling panels.

5. Conclusion

Based on a simple analysis, a pump energy saving at 40–45% will be achieved by using dynamic balancing and control valves for each device. The saving is due to a reduced number of static balancing and control valves and therefore in general a reduced head loss in the system. Reduced head loss means reduced pump energy consumption and a reduced pump size.



Energy consumption for pump: 6936 kWh/year



Server cooling
Static balancing design
24-2-2020 ver. 3
Kristian K. Hansen

Cooling load 180 kW
Flow 31,0 m³/h



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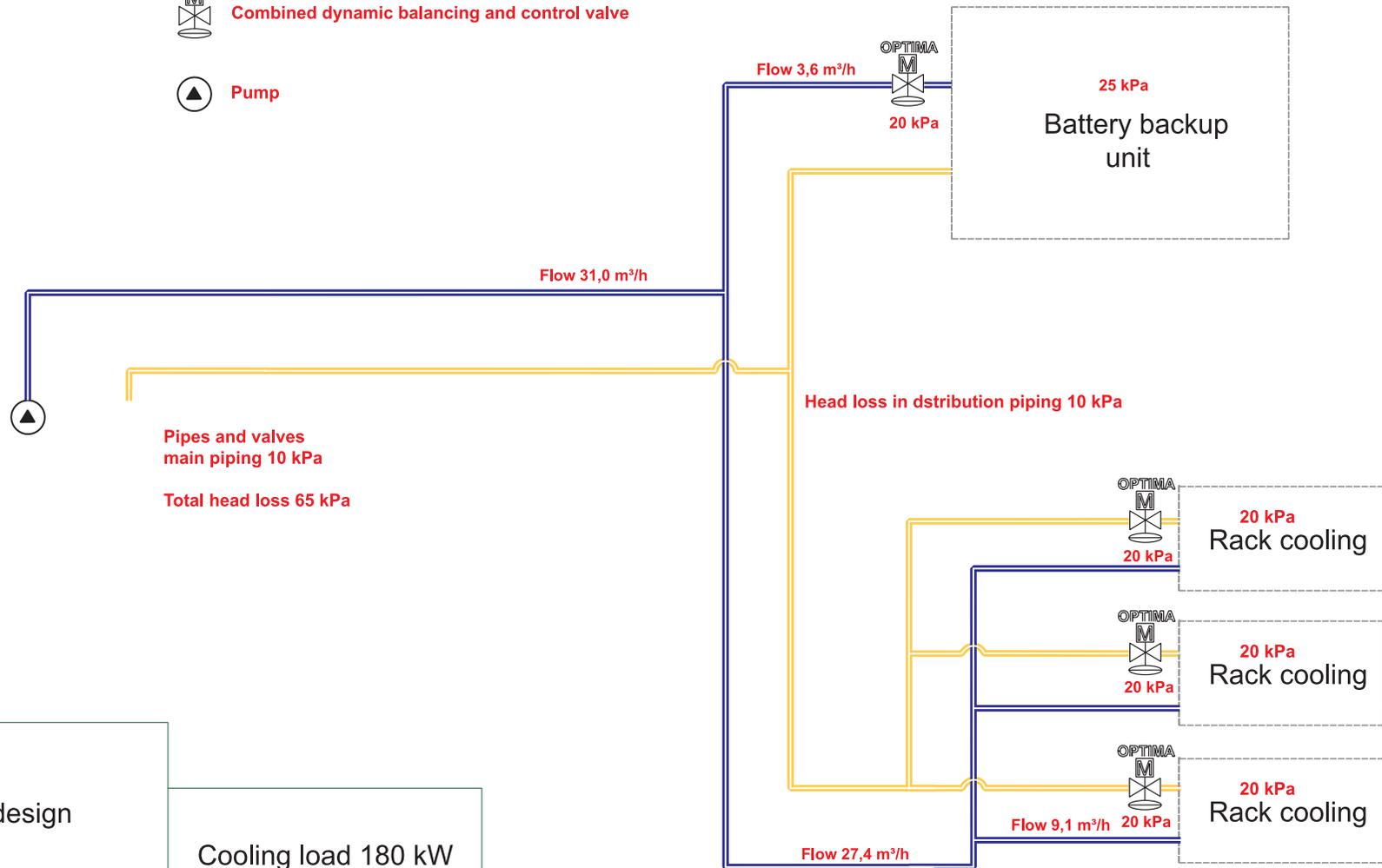
Energy consumption for
pump: 4181 kWh/year
Energy savings: 40%



Combined dynamic balancing and control valve



Pump

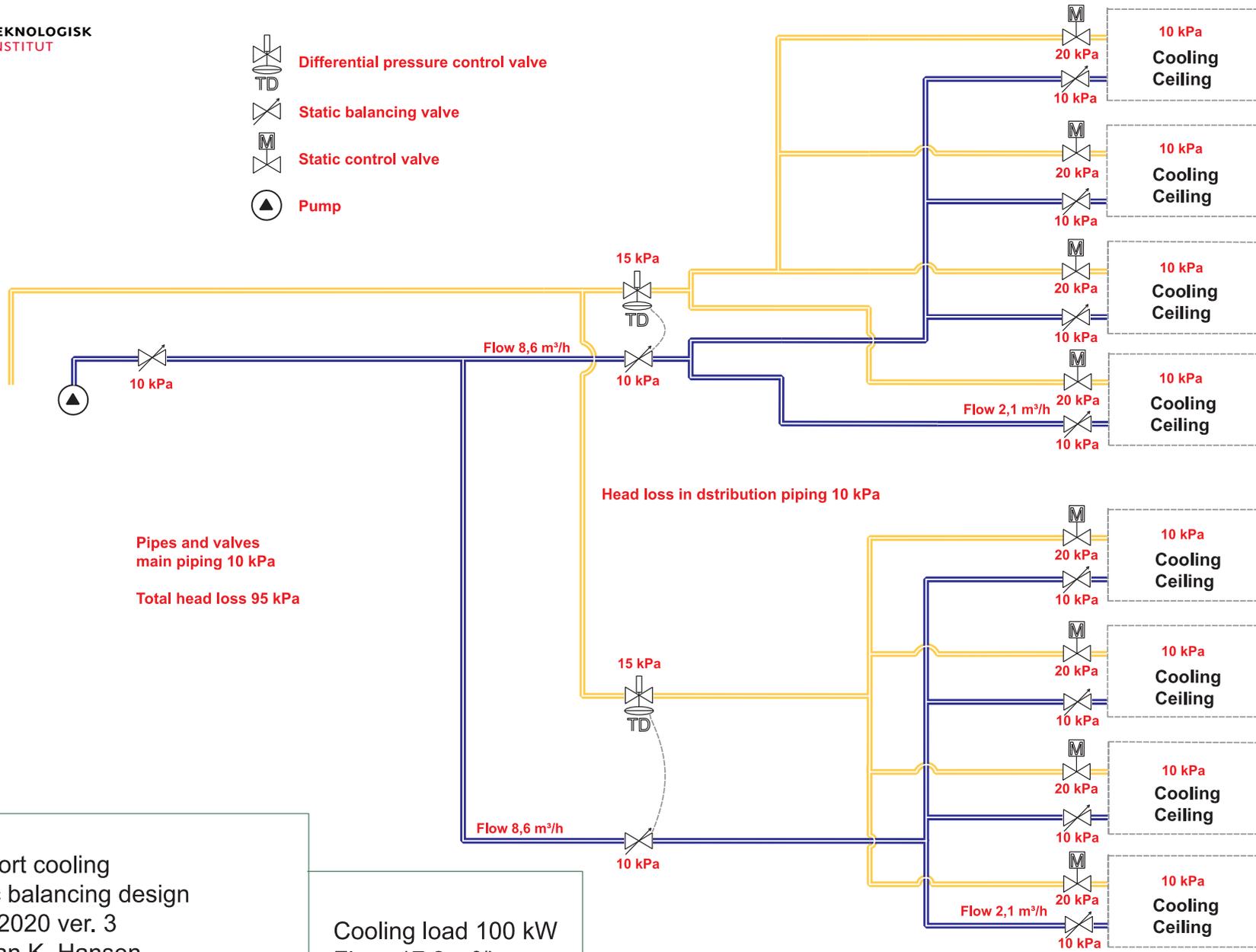
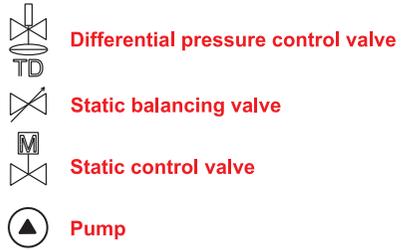


Server cooling
Dynamic balancing design
24-2-2020 ver. 3
Kristian K. Hansen

Cooling load 180 kW
Flow 31,0 m³/h



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Energy consumption for pump: 651 kWh/year

Pipes and valves main piping 10 kPa
Total head loss 95 kPa

Head loss in distribution piping 10 kPa

Comfort cooling
Static balancing design
27-2-2020 ver. 3
Kristian K. Hansen

Cooling load 100 kW
Flow 17,2 m³/h



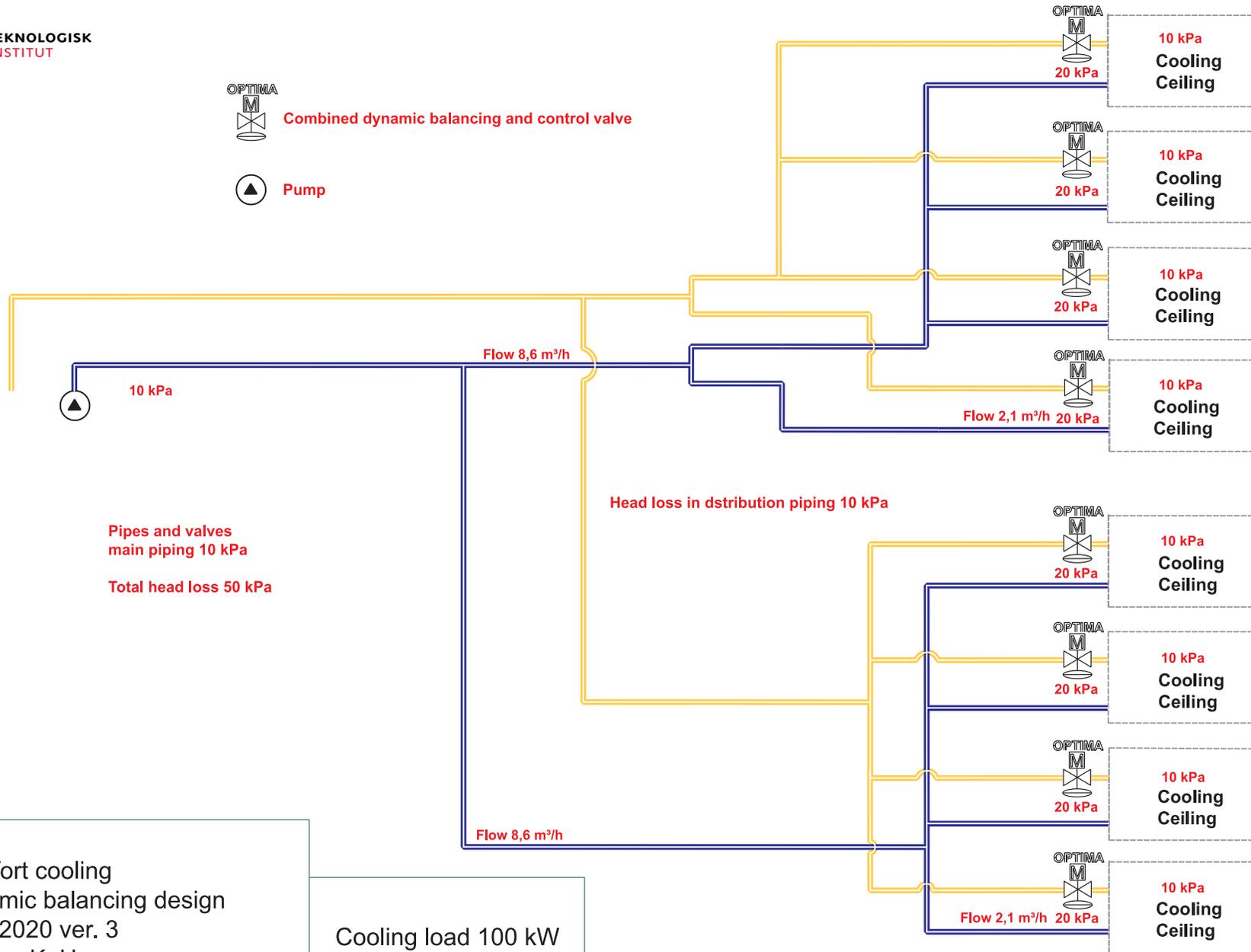
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OPTIMA
Combined dynamic balancing and control valve



Pump



Pipes and valves
main piping 10 kPa
Total head loss 50 kPa

Comfort cooling
Dynamic balancing design
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Cooling load 100 kW
Flow 17,2 m³/h

Energy consumption for
pump: 400 kWh/year
Energy savings: 40%



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